UNIVERSITY OF CALIFORNIA, BERKELEY
MECHANICAL ENGINEERING
ME106 Fluid Mechanics
NAME
2nd Test, S12 Prof S. Morris
Overall Mean: 132.5, STD: 37.6

1. (65)Abruptly closing an open book makes a bang as air is expelled rapidly from the gap between the pages. In the figure, each cover rotates around the axis $O$ with angular velocity $\pm \Omega$; the instantaneous angle between the covers is $2 \alpha$, and $(r, \phi)$ are plane polar coordinates.


Problem1
Mean: 43.2
STD: 16.5
(a) Assuming that $v_{\phi}=A r \sin 2 \phi$, use the boundary conditions and the continuity equation for incompressible flow

$$
\frac{1}{r} \frac{\partial\left(r v_{r}\right)}{\partial r}+\frac{1}{r} \frac{\partial v_{\phi}}{\partial \phi}=0
$$

to find $v_{r}$ in terms of $r, \phi, \Omega$ and $\alpha$. (A must not appear in your answer.) Note that $v_{r}$ must be finite at $r=0$.
(b) To find $A$, you will have imposed a boundary condition at $\phi=\alpha$; what is the name of this boundary condition?

## SOLUTION

(a) Substituting for $v_{\phi}$ into the continuity equation, we obtain

$$
\frac{1}{r} \frac{\partial\left(r v_{r}\right)}{\partial r}+2 A \cos 2 \phi=0 . \quad+15
$$

Multiplying by $r$ and integrating, we obtain

$$
r v_{r}=-A r^{2} \cos 2 \phi+G(\phi) ; \quad+15
$$

$G(\phi)$ is an arbitrary function of integration.
As stated, $v_{r}$ must be finite at $r=0$; consequently, $G(\phi)=0$.
To determine $A$, we note that at $\phi=\alpha, v_{\phi}=-\Omega r$; consequently,
+15
+15 Equate $\mathrm{V} \varphi=\Omega r$

$$
-\Omega r=A r \sin 2 \alpha \Rightarrow A=-\frac{\Omega}{\sin 2 \alpha} \text { Idea: } 10 \text {, Execution: } 5
$$

Hence

$$
v_{r}=\Omega r \frac{\cos 2 \phi}{\sin 2 \alpha}
$$

(b) Kinematic, or no penetration, boundary condition. $\quad+5$ if mentioned also "no slip" 4/5

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FULL CREDIT FOR CORRECT FINAL RESULT WITH COHERENT ARGUMENT
2. (65) (a) Water drains from the reservoir to atmospheric pressure through a pipe of length $L$ and diameter $d$. Assuming quasi-steady flow, and that the power loss in the pipe is given by $\frac{1}{2} \dot{m} f V^{2} L / d$, derive the expression giving the velocity $V$ in the pipe as a function of $d, L, g$, elevation change $H$, and friction factor $f$. For credit, you must include a sketch of your control volume, and you must explain briefly your assumptions.
(b) Hence find $V$ if $L=300 \mathrm{~km}, H=1 \mathrm{~km}, d=1 \mathrm{~m}$ and $f=0.03$. (You may assume that $g=10 \mathrm{~m}^{2} / \mathrm{s}$; for credit, your answer must be given as a decimal number and be accurate to within around 10\%.)


## SOLUTION

(a) Balance of mechanical energy on the control volume shown:

$$
\dot{m}\left[\frac{1}{2} V^{2}+(p / \rho)+g z\right]_{1}^{2}=\text { S.P. }- \text { power loss. } \quad(-10) \text { if not correct }
$$

Definition of the friction factor:

$$
\text { Power loss }=\frac{1}{2} \dot{m} f V^{2} \frac{L}{d}
$$

Simplifying the energy balance: $V_{1} \ll V_{2}=V ; p_{1}=p_{2}$ (atmospheric); $\dot{m}$ cancels from the energy
balance.
if not, (-5) if not, (-5)

$$
\frac{1}{2} V^{2}-g H=-\frac{1}{2} f V^{2} \frac{L}{d}
$$

Solving for $V^{2}$, we obtain

$$
\frac{1}{2}\left(1+f \frac{L}{d}\right)=g H .
$$

That is

$$
V=\sqrt{\frac{2 g H}{1+f(L / d)}}
$$

-minus sign under the square root without any notice, (-10)
(5)
(b) With the numbers given -Dimensional error with correct approach (40/60)

$$
V=\sqrt{\frac{2 \times 10 \times 10^{3}}{1+\left(0.03 \times 3 \times 10^{5}\right)}},=\sqrt{\frac{2 \times 10^{4}}{0.9 \times 10^{4}}}, \simeq \sqrt{2} \simeq 1.4 \mathrm{~m} / \mathrm{s}
$$

(-2) if it is not correct within around10\%

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3. (70) Water drains from a large tank through a small exit of area $A_{e} \ll A$ located within the tank interior far from all walls; as a result, $p$ is hydrostatic on the walls. Assuming that the jet velocity $V=\sqrt{2 g h}$, and using a balance momentum on the control volume shown, find the ratio $A_{j} / A_{e}$ of the jet area to the exit area.


## SOLUTION

According to the balance of vertical momentum, the resultant vertical force (downwards) is equal to the net flux of vertical momentum out of the control volume. Proper Mom. Bal.: $(+10)$
Because the tank is given to be large, the momentum flux through the upper surface of the control volume can be taken as negligibly small; the flux out through the jet is given by $\rho V^{2} A_{j}$. Mom. Flux.: (+10)

The resultant vertical force acting the water consists of two parts: its weight $\rho g A h$ (downward), and the resultant (upward) hydrostatic pressure force $\rho g\left(A-A_{e}\right)$ acting on the horizontal faces of the control surface. The resultant of these two is equal to $\rho g A_{e}$. Weight: (+20), Pressure: (+20)
Equating the momentum flux to the resultant force, we obtain $\rho V^{2} A_{j}=\rho g A_{e}$. Cancelling the common factor of $\rho$, then substituting for $V^{2}$, we obtain

$$
\frac{A_{j}}{A_{e}}=\frac{1}{2} . \quad \text { Result }(+10)
$$

The momentum balance requires the jet area to be half the exit area:

