

D a) No torque in the  $x$  or  $z$  by symmetry,

So we only need the  $y$ -component of  $\underline{I}$

or Because  $\underline{I} = \underline{r} \times \underline{F}$ , which means  $\underline{I}$  is perpendicular to both  $\underline{r}$  and  $\underline{F}$ , while  $\underline{r}$  and  $\underline{F}$  are on the  $x-z$  plane.  
So  $\underline{I}$  is just in  $y$  direction.

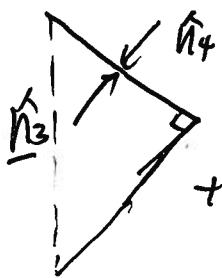
b).  $\underline{r} = (x, y, z) - (0, 0, z_1) = (x, y, z - z_1)$

There is a relationship between  $x$  and  $z$ :

$$\frac{x}{z_1 - z} = \tan 30^\circ = \frac{1}{\sqrt{3}} \quad x = \frac{z_1 - z}{\sqrt{3}}$$

$$\underline{r} = \left( \frac{z_1 - z}{\sqrt{3}} \right) \hat{x} + y \hat{y} + (z - z_1) \hat{z}$$

c). the normal vector that goes from  $P_3$  to upper section



$$\underline{n}_3 = \frac{1}{2} \hat{z} + \frac{\sqrt{3}}{2} \hat{x} = \cos 30^\circ \hat{x} + \sin 30^\circ \hat{z}$$

the normal vector goes from fluid  $P_4$  to upper section

$$\underline{n}_4 = -\underline{n}_3 = -\cos 30^\circ \hat{x} - \sin 30^\circ \hat{z} = -\frac{1}{2} \hat{z} - \frac{\sqrt{3}}{2} \hat{x}$$

d) Because the partition is sealed,  $P_L(z) \neq P_R(z)$   
 the pressure on the left side:  $P_L$

$$P_L = P_{atm} \quad z \geq 0$$

$$P_L = P_{atm} - \rho_3 g z \quad \bar{z} \leq z \leq 0$$

$$P_L = P_{atm} - \rho_3 g \bar{z} - \rho_1 g (z - \bar{z}) \quad z_B \leq z \leq \bar{z}$$

the pressure on the right side:  $P_R$

$$P_R = P_{atm} \quad z = z_4$$

$$P_R = P_{atm} - \rho_4 g (z - z_4) \quad \bar{z} \leq z \leq z_4$$

$$P_R = P_{atm} - \rho_4 g (\bar{z} - z_4) - \rho_1 g (z - \bar{z}) \quad z_B \leq z \leq \bar{z}$$

e)  $\vec{I} = \int dA \vec{r} \times [\hat{n}_3 P_L(z) + \hat{n}_4 P_R(z)]$

$$= \int dA \vec{r} \times \hat{n}_3 [P_L(z) - P_R(z)]$$

$$\vec{r} = \left( \frac{z_1 - z}{\sqrt{3}} \right) \hat{x} + y \hat{y} + (z - z_1) \hat{z}$$

$$\hat{n}_3 = \frac{1}{2} \hat{z} + \frac{\sqrt{3}}{2} \hat{x}$$

$$\begin{aligned} \vec{r} \times \hat{n}_3 &= \left( \frac{z_1 - z}{\sqrt{3}} \hat{x} + y \hat{y} + (z - z_1) \hat{z} \right) \times \left( \frac{1}{2} \hat{z} + \frac{\sqrt{3}}{2} \hat{x} \right) \\ &= \frac{1}{2} \left[ \frac{z - z_1}{\sqrt{3}} \hat{y} + \hat{y} \cdot \sqrt{3}(z - z_1) \right] = \frac{(z - z_1)}{2} \frac{4}{\sqrt{3}} \hat{y} \end{aligned}$$

P3

$$P_L(z) = \rho_{atm} - \rho_3 g z, \quad P_R(z) = \rho_{atm} - \rho_4 g (z - z_4) \quad \hat{z} < z \leq z_4$$

$$P_L(z) - P_R(z) = \rho_4 g z - \rho_3 g z + \rho_4 g z_4 = g [(\rho_4 - \rho_3) z - \rho_4 z_4]$$

$$\underline{P} = \int dA \frac{2(z-z_1)}{\sqrt{3}} \hat{j} \cdot \hat{g} [(\rho_4 - \rho_3) z - \rho_4 z_4] \hat{y}$$

$$= \frac{2g}{\sqrt{3}} \int dA [(\rho_4 - \rho_3) z - \rho_4 z_4] (z - z_1) \hat{x}$$

$$dA = L \cdot dz / \cos 30^\circ = dz L \frac{2}{\sqrt{3}}$$

$$\hat{y} \cdot \underline{P} = \frac{2g}{\sqrt{3}} \frac{2L}{\sqrt{3}} \int_{\bar{z}}^{z_1} dz (z - z_1) [(\rho_4 - \rho_3) z - \rho_4 z_4]$$

$$= \frac{4}{3} g L \int_{\bar{z}}^{z_1} dz [(\rho_4 - \rho_3) z^2 + (\rho_3 z_1 - \rho_4 z_1 - \rho_4 z_4) z + \rho_4 z_1 z_4]$$

$$= \frac{4}{3} g L \left[ \int_{\bar{z}}^{z_1} (\rho_4 - \rho_3) \frac{z^3}{3} \right]$$

$$= \frac{4}{3} g L [(\rho_4 - \rho_3) \frac{z_1^3 - \bar{z}^3}{3} + (\rho_3 z_1 - \rho_4 z_1 - \rho_4 z_4) \frac{z^2}{2} + \rho_4 z_1 z_4 z]$$

$$= \frac{\rho_3 - \rho_4}{6} z_1^3 + \frac{\rho_3 - \rho_4}{3} \bar{z}^3 + \frac{\rho_4 - \rho_3}{2} z_1 \bar{z}^2 + \frac{\rho_4}{2} z_4 z_1^2 + \frac{\rho_4}{2} z_4 \bar{z}^2 - \rho_4 z_1 z_4 z$$

$$2). \quad \vec{I} = \int dA \cdot \hat{z} \times \hat{n}_1 (P_L - P_R)$$

We calculate the torque in  $y$  direction, which is non-zero  
 $\hat{n}_1 = \cos 60^\circ \hat{x} - \sin 60^\circ \hat{z} = \frac{1}{2} \hat{x} - \frac{\sqrt{3}}{2} \hat{z}$

$$\vec{r} = (x, y, z) - (0, 0, z_2) = (x, y, z - z_2)$$

\*the relationship between  $x$  and  $z$ :

$$\tan 60^\circ = \frac{x}{z - z_2} = \sqrt{3} \quad x = \sqrt{3}(z - z_2)$$

$$\begin{aligned} \vec{r} \times \hat{n}_1 &= (\sqrt{3}(z - z_2) \hat{x} + y \hat{y} + (z - z_2) \hat{z}) \times \left( \frac{1}{2} \hat{x} - \frac{\sqrt{3}}{2} \hat{z} \right) \\ &= \left[ -\frac{3}{2}(z_2 - z) \hat{y} + \frac{z - z_2}{2} \hat{y} \right] = 2(z - z_2) \hat{y} \end{aligned}$$

$$\begin{aligned} P_L - P_R &= \rho g \hat{z} - \rho_3 g \hat{z} - \rho_1 g (z - \hat{z}) - \rho g \hat{z} + \rho_4 g (\hat{z} - z_4) + \rho_1 g (z - \hat{z}) \\ &= (\rho_4 g - \rho_3 g) \hat{z} - \rho_4 g z_4 = g [(\rho_4 - \rho_3) \hat{z} - \rho_4 z_4] \end{aligned}$$

$$\begin{aligned} \hat{y} \cdot \vec{I} &= \int dA \cdot 2(z - z_2) g [(\rho_4 - \rho_3) \hat{z} - \rho_4 z_4] \\ &= 2g [(\rho_4 - \rho_3) \hat{z} - \rho_4 z_4] \int \cdot [(\rho_4 - \rho_3) \hat{z} - \rho_4 z_4] dA \end{aligned}$$

$$dA = L dz / \sin 30^\circ = 2L dz$$

$$\hat{y} \cdot \vec{I} = 4gL [(\rho_4 - \rho_3) \hat{z} - \rho_4 z_4] \int_{z_2}^{\hat{z}} (z - z_2) dz$$

PF

$$\underline{P}_2 = 4gLT [(\rho_4 - \rho_3)\bar{z} - \rho_4 z_4] \frac{(\bar{z} - z_2)^2}{2} / \bar{z}$$

$$= 4gLT (\rho_4 - \rho_3)\bar{z} - \rho_4 z_4) \frac{(\bar{z} - z_2)^2}{2} \hat{y} = 2gL T (\rho_4 - \rho_3)\bar{z} - \rho_4 z_4] (\bar{z} - z_2)$$

$$3) \quad \underline{P}_1 = \underline{P}_2 + \gamma_{12} \times \underline{F}$$

$$\gamma_{12} = (0, 0, z_2 - z_1)$$

$$\underline{F} = \int d\Omega (\rho_L - \rho_R) \cdot \hat{n}$$

$$= \int 2L dz g [(\rho_4 - \rho_3)\bar{z} - \rho_4 z_4] \cdot \left( \frac{1}{2}\hat{x} - \frac{\sqrt{3}}{2}\hat{z} \right)$$

$$\begin{aligned} \underline{F} \cdot \hat{x} &= Lg \int_{z_2}^{\bar{z}} T(\rho_4 - \rho_3)\bar{z} - \rho_4 z_4 dz \\ &= Lg T(\rho_4 - \rho_3)\bar{z} - \rho_4 z_4] (\bar{z} - z_2) \end{aligned}$$

$$\underline{\gamma}_{12} \times (\underline{F} \cdot \hat{x}) = + (z_2 - z_1)(\bar{z} - z_2) Lg T(\rho_4 - \rho_3)\bar{z} - \rho_4 z_4] \hat{y}$$

~~Because~~ The relationship between  $z_1$  and  $z_2$

$$(z_1 - \bar{z}) \tan 30^\circ = \frac{\bar{z} - z_2}{\tan 30^\circ} \Rightarrow 3(\bar{z} - z_2) = (z_1 - \bar{z})$$

$$\hat{y} \cdot \underline{P}_1 = (\underline{P}_2 + \gamma_{12} \times \underline{F}) \hat{y}$$

$$\begin{aligned} &= [(\rho_4 - \rho_3)\bar{z} - \rho_4 z_4] g_L T (\bar{z} - z_2) [2(\bar{z} - z_2) + z_2 - \bar{z}] \\ &= E(\rho_4 - \rho_3)\bar{z} - \rho_4 z_4 g_L (\bar{z} - z_2) [-(\bar{z} - z_2)] \\ &= - \underline{P}_2 \end{aligned}$$

4) the torque around point I is zero

P6.

$$\begin{aligned} & \frac{\rho_3 - \rho_4}{6} z_1^3 + \frac{\rho_3 - \rho_4}{3} \bar{z}^3 + \frac{\rho_4 - \rho_3}{2} z_1 \bar{z}^2 + \frac{\rho_4}{2} z_4 z_1^2 + \frac{\rho_4}{2} z_4 \bar{z}^2 - \rho_4 z_1 z_4 \bar{z} \\ = & 2g L [(\rho_4 - \rho_3) \bar{z} - \rho_4 z_4] (z - z_2)^2 \end{aligned}$$