

Prob. 1 a) Work =  $\int_a^d p dV$

$$W = \int_a^d \frac{C}{V^\gamma} dV$$

$$W = \frac{C}{1-\gamma} \cdot V^{1-\gamma} \Big|_{V_c}^{V_d} = \frac{C}{1-\gamma} (V_d^{1-\gamma} - V_c^{1-\gamma})$$

$$W = \frac{P_c V_c^\gamma}{1-\gamma} \cdot \left[ \left( V_c \cdot \left( \frac{P_c}{P_d} \right)^{1/\gamma} \right)^{1-\gamma} - V_c^{1-\gamma} \right] = \frac{P_c V_c}{1-\gamma} \left[ \left( \frac{P_c}{P_d} \right)^{\frac{1-\gamma}{\gamma}} - 1 \right]$$

$$W = \frac{P_c V_c}{1-\gamma} \left[ \left( \frac{P_c}{P_d} \right)^{\frac{1-\gamma}{\gamma}} - 1 \right]$$

For adiabatic process:  $pV^\gamma = \text{constant}$   
 $\therefore P_c V_c^\gamma = \text{constant} = C = P_d V_d^\gamma$   
 $P = C/V^\gamma$

b) efficiency:  $\epsilon = \frac{W}{Q_H} = \frac{Q_H - Q_L}{Q_H} = 1 - \frac{Q_L}{Q_H}$

$$\gamma = (d_f + z) / d_f$$

$$d_f / z = 1 / (\gamma - 1)$$

1<sup>st</sup> - law of thermo:  $T ds = dQ = dE + p dV$

$$\therefore \Delta Q = (\gamma - 1)^{-1} N k_B \cdot \Delta T + p \cdot \Delta V \text{ for isobaric processes.}$$

$$Q_H = \Delta Q_{cb} = (\gamma - 1)^{-1} N k_B (T_c - T_b) + P_b (V_c - V_b)$$

$$= (\gamma - 1)^{-1} P_b (V_c - V_b) + P_b (V_c - V_b) = \frac{\gamma \cdot P_b (V_c - V_b)}{\gamma - 1}$$

$$Q_L = -\Delta Q_{da} = \frac{\gamma \cdot P_a \cdot (V_d - V_a)}{\gamma - 1} \text{ (same approach as above).}$$

Adiabats:  $P_a V_a^\gamma = P_b V_b^\gamma$   
 $V_a = V_b \cdot \left( \frac{P_b}{P_a} \right)^{1/\gamma}$

$$P_c V_c^\gamma = P_d V_d^\gamma$$

$$V_c = V_d \left( \frac{P_d}{P_c} \right)^{1/\gamma} \Leftrightarrow V_d = V_c \left( \frac{P_b}{P_a} \right)^{1/\gamma}$$

$$\therefore \epsilon = 1 - \frac{\gamma \cdot P_a \cdot (V_d - V_a)}{\gamma \cdot P_b (V_c - V_b)} = 1 - \frac{P_a \cdot \left( \frac{P_b}{P_a} \right)^{1/\gamma} \cdot (V_c - V_b)}{P_b \cdot (V_c - V_b)}$$

$$= 1 - \left( \frac{P_a}{P_b} \right)^{\frac{\gamma-1}{\gamma}} = \epsilon$$

\* Note: There should be a  $(\gamma-1)$  in top + bottom that cancel.

2.



$$g(r) = \frac{\rho_0}{r} \quad \int d^3r g(r) = \rho_0 (4\pi) \int_0^R \frac{r^2}{r} dr = \rho_0 (4\pi) \int_0^R r dr = \frac{\rho_0 (4\pi) R^2}{2} = Q_0$$

$$\text{const} = \rho = Q_0 = \boxed{\rho_0 = \frac{2Q}{4\pi R^2} = \frac{Q}{2\pi R^2}} \quad (3)$$

at

$$E_{\text{out}} = \frac{kQ}{r^2} = \boxed{\frac{1}{4\pi\epsilon_0} \frac{Q}{r^2}} \quad (\text{out}) \quad (3)$$

$$U_{\text{out}} = \int \frac{1}{2} \epsilon_0 |E_{\text{out}}|^2 d^3r = \frac{1}{2} \epsilon_0 \frac{1}{(4\pi\epsilon_0)^2} Q^2 (4\pi) \int_R^\infty dr \frac{r^2}{r^4}$$

$$= \frac{1}{2} \frac{Q^2}{4\pi\epsilon_0} \int_R^\infty \frac{dr}{r^2} = \frac{1}{2} \frac{Q^2}{4\pi\epsilon_0} \left(-\frac{1}{r}\right)_R^\infty = \boxed{\frac{1}{2} \frac{Q^2}{4\pi\epsilon_0} \frac{1}{R}} \quad (3)$$

I<sub>in</sub>

$$\oint \vec{E} \cdot d\vec{a} = 4\pi R^2 E = \frac{Q_{\text{in}}}{\epsilon_0}$$

$$E = \frac{Q_{\text{in}}}{4\pi\epsilon_0 R^2}$$

$$Q_{\text{in}} = \int_0^r r^2 g(r) dr = 4\pi \rho_0 \int_0^r r dr = 4\pi \left(\frac{Q}{2\pi R^2}\right) \int_0^r r dr$$

$$= \frac{2Q}{R^2} \frac{r^2}{2} = \frac{Q r^2}{R^2} \quad (4)$$

$$\boxed{E = \frac{Q}{4\pi\epsilon_0 R^2}} \quad (\text{in}) \quad (3)$$

$$U_{\text{in}} = \frac{1}{2} \epsilon_0 \int |\vec{E}|^2 d^3r = \frac{1}{2} \epsilon_0 \frac{Q^2}{(4\pi\epsilon_0)^2} R^2 \frac{4\pi R^3}{3} = \frac{1}{2} \frac{Q^2}{4\pi\epsilon_0} \frac{1}{3R} = \boxed{\frac{1}{2} \frac{Q^2}{12\pi\epsilon_0 R}} \quad (3)$$

Total

$$U = \frac{1}{2} \frac{Q^2}{4\pi\epsilon_0} \left[ \frac{1}{R} + \frac{1}{3R} \right] = \boxed{\frac{Q^2}{6\pi\epsilon_0 R}}$$

Errors

- (+) (only) for  $U = QV$
- (+) (only) for  $U = \sum_{i \neq j} U_{ij} = \frac{kQ^2}{r_{ij}}$
- (-) (only) if relates  $U = \frac{1}{2} \epsilon_0 \int |\vec{E}|^2$ , but nothing else



3



a) inside

Just:  $\oplus$  Ans:  $\oplus$

(wrong:  $\ominus$ )

b)  $\vec{E} = \frac{\sigma}{\epsilon_0} \hat{z}$

Just:  $\oplus$  Ans:  $\oplus$  (-1 for vector)

c)  $\frac{p}{V} = \frac{Q \times d}{V} = \frac{Q \times A \times a}{A \times a} = Q$

(3) (-1 for vector)

Pointing up!

$\oplus$  if wrong but makes some sense

$\oplus$  if  $Vol = A \times t$  instead

$\ominus$  if wrong formula, no idea...

Problem 4

(a) Charges are at rest, find electric force.

$$\text{Gauss' Law: } \int \vec{E} \cdot d\vec{A} = \frac{Q_{enc}}{\epsilon_0} \rightarrow E_{cyl}(2\pi r l) = \frac{\lambda l}{\epsilon_0}$$

$$E = \frac{\lambda}{2\epsilon_0 \pi r} \rightarrow \vec{F} = q\vec{E} = \frac{q\lambda}{2\epsilon_0 \pi r} \hat{r}$$

(b) Moving charge creates magnetic field. Use Lorentz force law for net force

$$\text{Ampere's Law: } \int \vec{B} \cdot d\vec{l} = \mu_0 I_{enc} \rightarrow B(2\pi r) = \mu_0 I \rightarrow \vec{B} = \frac{\mu_0 I}{2\pi r} \hat{\theta}$$

$$I = \frac{dq}{dt} = \frac{dq}{dx} \frac{dx}{dt} = \lambda v \rightarrow \vec{B} = \frac{\mu_0 \lambda v}{2\pi r} \hat{\theta}$$

$$\text{Lorentz Force Law: } \vec{F} = q(\vec{E} + \vec{v} \times \vec{B}) = q(E\hat{r} + (v\hat{z}) \times (B\hat{\theta})) = q(E - vB)\hat{r}$$

$$\vec{F} = q \left( \frac{\lambda}{2\epsilon_0 \pi r} - \frac{\mu_0 \lambda v^2}{2\pi r} \right) \hat{r}$$

$$\text{Eliminate } \mu_0: \quad c = \frac{1}{\sqrt{\epsilon_0 \mu_0}} \rightarrow \mu_0 = \frac{1}{\epsilon_0 c^2}$$

$$\vec{F} = \frac{q\lambda}{2\epsilon_0 \pi r} \left( 1 - \frac{v^2}{c^2} \right) \hat{r}$$

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 Problem 3 Solution

a. The back EMF of an inductor is  $\mathcal{E} = -L \frac{dI}{dt}$ , so in steady state the solenoid will act like a wire with internal resistance. (1 point)

$$R = \rho \frac{l}{A}$$

$$l = 2\pi r_s N = 2\pi r_s \ell_s$$

$$A = wh$$

$$\Rightarrow R = \frac{\rho \ell_s 2\pi r_s}{wh}$$

(1 point)

(1 point)

(1 point)

b.  $L = \frac{\Phi}{I}$

The magnetic field inside can be found using ampere's law, and approximating the solenoid to be a perfect solenoid, i.e. uniform surface current along cylindrical axis  $\ell_s \gg r_s$ .

$$B = \mu_0 \frac{N}{\ell_s} I$$

$$\Rightarrow \Phi = N A_s B = \mu_0 N^2 A_s I$$

$$\Rightarrow L = \frac{\mu_0 N^2 A_s \ell_s}{w^2}$$

(2 points)

(2 points)

c. The time constant can be derived by treating this as an RC circuit for wire resistance. Laws are given by

$$\mathcal{E}_0 - IR - L \frac{dI}{dt} = 0$$

$$\Rightarrow \frac{\mathcal{E}_0}{R} - I - \frac{L}{R} \frac{dI}{dt} = 0$$

$$\Rightarrow \tau = \frac{L}{R}$$

It was not necessary to plug in b and a

(3 points)

$$\tau = \frac{\pi r_s^2 \mu_0 \ell_s}{w^2} \frac{\mu_0 N^2 \ell_s}{2\pi r_s w}$$

(2 points)

$$\frac{\mu_0 N^2 \ell_s}{4\pi w}$$

(2 points)

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 Problem 6 Solution:

$$Q = \int dQ = \int \frac{dQ}{dt} dt = \int I dt$$

(3 points)

$$I = \frac{\mathcal{E}}{R} = \frac{1}{R} \frac{d\Phi}{dt} \Rightarrow Q = \int \frac{1}{R} \frac{d\Phi}{dt} dt$$

(2 points)

$$= \frac{1}{R} \int d\Phi$$

(2 points)

$$= \frac{1}{R} \Delta\Phi$$

to maximize the charge that flows, clearly the change in flux must be largest a rotating wire pair in perspective with the magnetic field.

$$\Rightarrow Q = \frac{1}{R} (\pi r^2 B - 0)$$

(2 points)

the number of electrons then is

$$N_e = \frac{Q}{e} = \frac{\pi r^2 B}{Re}$$

(1 point)

where  $e$  is the charge of one electron.

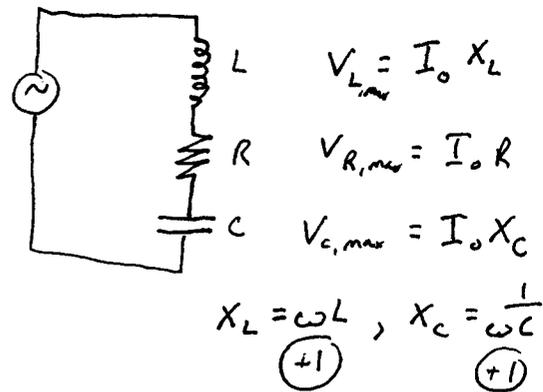
Note that it is not necessary to assume that the process happens at constant angular velocity, nor is it necessary to approximate

$$\frac{d\Phi}{dt} \approx \frac{\Delta\Phi}{\Delta t}$$

# Problem 7

[10 pts] a)  $V = V_0 \cos(\omega t + \phi)$

First, solve for  $I_0$  (amplitude of current)



amplitude of voltage of power source

$\hookrightarrow V_0 = I_0 \cdot \underset{\substack{\uparrow \\ \text{impedance}}}{Z}$  where  $Z = \sqrt{R^2 + (X_L - X_C)^2}$

$\Rightarrow I_0 = \frac{V_0}{Z} = \frac{V_0}{\sqrt{R^2 + (X_L - X_C)^2}}$

amplitude of voltage across capacitor is:

$V_{C, \max} = I_0 X_C = \left( \frac{V_0}{\sqrt{R^2 + (X_L - X_C)^2}} \right) X_C = \left( \frac{X_C}{\sqrt{R^2 + (X_L - X_C)^2}} \right) V_0$

$\Rightarrow V_{C, \max} = \frac{V_0}{\omega C \sqrt{R^2 + \left( \omega L - \frac{1}{\omega C} \right)^2}}$

[5 pts] b) at resonance,  $\omega = \frac{1}{\sqrt{LC}} \Rightarrow X_L = X_C = \sqrt{\frac{L}{C}}$

so  $V_{C, \max} = \frac{X_C}{R} V_0 = \frac{1}{R} \sqrt{\frac{L}{C}} V_0$

$\Rightarrow \frac{V_{C, \max}}{V_0} = \left( \frac{L}{R^2 C} \right)^{1/2} > 1$  since  $R^2 C < L$