

* -5 ATLEAST FOR
ANY MATHEMATIC ERRORS
IN WORK

* NO CREDIT FOR
DIMENSIONALLY INCORRECT
WORK

UNIVERSITY OF CALIFORNIA, BERKELEY
MECHANICAL ENGINEERING
ME106 Fluid Mechanics
1st Test, S08 Prof S. Morris

NAME SOLUTIONS

- 1.(65) (a) Find the fluid acceleration \mathbf{a} for plane stagnation point flow in which the velocity is given by the expression $\mathbf{V} = cx\mathbf{i} - cy\mathbf{j}$ (the constant $c > 0$).

EITHER

$$\frac{d\tilde{\mathbf{V}}}{dt} = \frac{d}{dt}(cx\mathbf{i}) - \frac{d}{dt}(cy\mathbf{j}) \\ = c\mathbf{i} \frac{dx}{dt} - c\mathbf{j} \frac{dy}{dt}$$

Exam stats
Mean: 124.8/200
St. Dev: 37.1
(c_1, c_2 const in mag. & direction)

But $\frac{dx}{dt} = c_x, \frac{dy}{dt} = -c_y \Rightarrow$

$$\frac{d\tilde{\mathbf{V}}}{dt} = c^2(\mathbf{i}_x + \mathbf{j}_y)$$

or. $\tilde{\mathbf{V}} = u\mathbf{i}_x + v\mathbf{j}_y$

$$\frac{d\tilde{\mathbf{V}}}{dt} = u \frac{\partial \tilde{\mathbf{V}}}{\partial x} + v \frac{\partial \tilde{\mathbf{V}}}{\partial y} \quad \therefore \frac{\partial \tilde{\mathbf{V}}}{\partial t} = 0$$

$$\frac{\partial \tilde{\mathbf{V}}}{\partial x} = c\mathbf{i}, \frac{\partial \tilde{\mathbf{V}}}{\partial y} = -c\mathbf{j} \Rightarrow$$

$$\frac{d\tilde{\mathbf{V}}}{dt} = (c_x)(c_y) + (-c_y)(-c_x) \\ \Rightarrow \frac{\partial \tilde{\mathbf{V}}}{\partial t} = c^2(\mathbf{i}_x + \mathbf{j}_y)$$

lost points for:

math errors, -5

did not underline unit vectors, -5

confuse vectors and scalars, -10

Pr. 1 stats
Mean: 57.4/65
St Dev: 12.1

- (b) By considering the stagnation streamline, explain why $\mathbf{a} \neq 0$ in this flow.

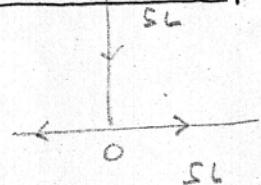
On the branch $x=0$ $\tilde{\mathbf{V}} = -cy\mathbf{j}$

Velocity of FP moving along SL to origin
decreases with $y \Rightarrow \mathbf{a} \neq 0$.

No credit for arguments that:

- velocity changes throughout flow
- using a w/o physical reasoning

IN BLOCK LETTERS PRINT YOUR NAME ON THIS PAGE



Pr. 2 Stats

Mean: 40.6 / 65

St. Dev: 22, 1

2. (65) The vector field $\mathbf{V} = -\frac{1}{2}cr\hat{\mathbf{r}} + v(r, t)\hat{\theta} + cz\hat{\mathbf{k}}$ ($c > 0$, constant) represents a vortex that is being stretched in the axial direction. For this flow, the fluid acceleration is given by the expression

$$\mathbf{a} = \left(\frac{1}{4}c^2r - \frac{v^2}{r} \right) \hat{\mathbf{r}} + \left(\frac{\partial v}{\partial t} - \frac{1}{2}c \frac{\partial(rv)}{\partial r} \right) \hat{\theta} + c^2z\hat{\mathbf{k}}$$

(You are not required to show that.) Find the partial differential equation satisfied by the function $v(r, t)$. (You are not asked to solve it.)

Given. In cylindrical polar coordinates r, θ, z , if $\mathbf{F} = f_r\hat{\mathbf{r}} + f_\theta\hat{\theta} + f_z\hat{\mathbf{k}}$ is an arbitrary vector, then

$$\nabla \times \mathbf{F} = \frac{1}{r} \begin{vmatrix} \hat{\mathbf{r}} & \frac{r\hat{\theta}}{\partial r} & \hat{\mathbf{k}} \\ \frac{\partial}{\partial r} & \frac{\partial}{\partial \theta} & \frac{\partial}{\partial z} \\ f_r & rf_\theta & f_z \end{vmatrix}$$

Euler's equation for constant p is satisfied \Leftrightarrow

$$\boxed{\nabla \times \mathbf{a} = 0} + 20$$

$$r \nabla \times \mathbf{a} = \begin{vmatrix} \hat{\mathbf{r}}, r\hat{\theta}, \hat{\mathbf{k}} \\ \frac{\partial}{\partial r}, 0, 0 \\ \frac{c^2r}{4} - \frac{v^2}{r}, r\left\{ \frac{\partial v}{\partial t} - \frac{1}{2}c \frac{\partial}{\partial r}(rv) \right\}, c^2z \end{vmatrix} = \hat{\mathbf{r}} - r\hat{\theta} \frac{\partial}{\partial r} \left(\frac{\partial v}{\partial t} - \frac{1}{2}c \frac{\partial}{\partial r}(rv) \right) + 0\hat{\mathbf{k}}$$

$\leftarrow + 30 \quad \text{Expanding } \nabla \times \mathbf{a} = 0$

$$\text{so } \nabla \times \mathbf{a} = 0 \quad \Leftrightarrow \quad \frac{\partial}{\partial r} \left(\frac{\partial v}{\partial t} - \frac{1}{2}c \frac{\partial}{\partial r}(rv) \right) = 0 \quad A.$$

$$\underline{\underline{\text{or}}} \quad \boxed{\frac{\partial^2}{\partial t^2}(rv) - \frac{1}{2}c r \frac{\partial^2}{\partial r^2}(rv) = f(t)} \quad B.$$

Either A. or B. is acceptable. + 15 for complete and correct solution.

Point deductions:

- * If you attempted to use Euler's equation and plugged in CORRECTLY, + 30
- Did not see $\frac{\partial v}{\partial \theta} + \frac{\partial v}{\partial z} = 0$ - 15

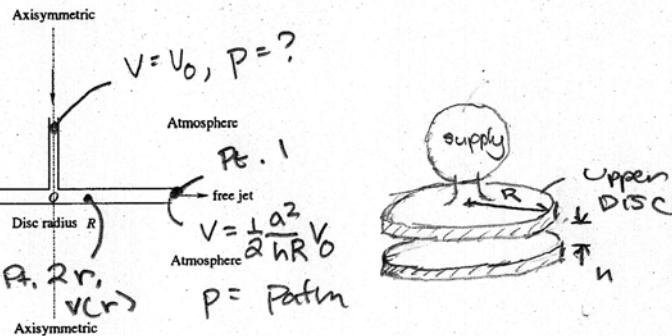
- Missing r terms, - 5

- 70
 3. (45) The figure shows the side view of two discs each of radius R , and separated by fixed distance h . Air enters the gap between the discs with speed V_0 through the supply tube of radius a , flows radially and leaves as a free jet into the atmosphere. Atmospheric pressure is p_a . Within the gap, the speed V varies with distance r from the axis according to the rule

$$V = \begin{cases} \frac{1}{2} \frac{r}{h} V_0 & \text{if } r < a \\ \frac{1}{2} \frac{a^2}{hr} V_0 & \text{if } r > a \end{cases}$$

(You are not required to show that.) The pressure within the supply tube is unknown; it is not atmospheric.

* If you used Bernoulli w/ one pt @ supply WITH $P = P_{atm}$, you got a max of +5 for (a)



- (40) (a) Using the Bernoulli equation, find the pressure p within the gap as a function of r , ρ , V_0 , h and a . Sketch p as a function of r showing clearly any maxima, minima and zeros. (You need to consider the cases $r < a$, $r > a$ separately.)

BE along SL from r to exit

$$\Rightarrow \frac{1}{2} p V^2(r) + p(r) = \frac{1}{2} p V_e^2 + p_a \quad \left. \begin{array}{l} p_f \text{ at } 2 \\ p \text{ at } 1 \end{array} \right\}$$

$$\Rightarrow p(r) - p_a = \frac{1}{2} p V_e^2 \left[1 - \frac{V^2(r)}{V_e^2} \right]$$

+20 for properly using Bernoulli properly.

This includes those who tried to find P_{supply}

But

$$V_e = \frac{1}{2} \frac{a^2}{hR} V_0$$

$$\frac{V}{V_e} = \begin{cases} \frac{Rr}{a^2} & , r < a \\ \frac{R}{r} & , r > a \end{cases}$$

$r < a$

$r > a$

\Rightarrow

$$\frac{p(r) - p_a}{\frac{1}{2} p V_e^2} = \begin{cases} 1 - \frac{R^2}{a^2} \frac{r^2}{r^2} + 5 & , r < a \\ 1 - \frac{R^2}{r^2} + 5 & , r > a \end{cases}$$

1s08-3

BOXED

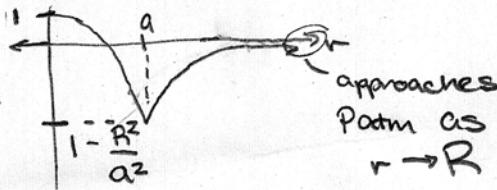
EQU

GIVE THE
SOLN

since $R > a$

$$\frac{R}{a} > 1$$

$$\frac{p(r) - p_a}{\frac{1}{2} p V_e^2} = 1 - \frac{R^2}{a^2}$$



approaches P_{atm} as $r \rightarrow R$

+5 for correct plot

+5 for correct labeling + comments

(20) (b) Noting that the flow is axisymmetric, derive the integral expressing the force F exerted by the air on both sides of the lower disc in terms of the pressure difference $p(r) - p_a$.

REQUIRED FOR FULL CREDIT

Area element is a ring of radius r , thickness dr or $dA = r dr d\theta$ $p(r) 2\pi r dr$

Vertical force on $dA = 2\pi [p_a - p(r)] r dr$

Force upward on lower disc = $2\pi \int_0^R [p_a - p(r)] r dr$

(c) Hence show that F is given by the expression -10 for failing to consider p_a underneath

$$F = \frac{1}{4} \pi \rho \frac{a^4}{h^2} V_0^2 \left(\ln \frac{R}{a} - \frac{1}{4} \right).$$

Explain physically why, despite the presence of a stagnation point at O , the force is upwards if $R \gg a$.

$$\begin{aligned} \frac{F}{\rho \pi V_0^2} &= - \int_0^R \left(1 - \frac{V^2}{V_0^2} \right) r dr \\ &= - \int_0^a \left(1 - \frac{R^2}{a^2 + r^2} \right) r dr - \int_a^R \left(1 - \frac{R^2}{r^2} \right) r dr \\ &= - \left[\frac{1}{2} r^2 - \frac{R^2}{4a^4} r^4 \right]_0^a - \left[\frac{1}{2} r^2 - R^2 \ln r \right]_a^R \\ &= R^2 \ln \frac{R}{a} - \frac{1}{4} R^2 \end{aligned}$$

+5
• Requires full + correct integration of correct v function

i.e.

$$\frac{F}{\frac{1}{4} \rho \pi \frac{a^4}{h^2} V_0^2} = R^2 \left(\ln \frac{R}{a} - \frac{1}{4} \right)$$

$\frac{F}{\frac{1}{4} \rho \pi \frac{a^4}{h^2} V_0^2} = \ln \frac{R}{a} - \frac{1}{4}$

Subst for V_0

END

+5

1s08-4

Although near stagnation $p(r) > p_a$, over most of the disc is $p(r) < p_a$. Consider mass conservation. For $r > a$, as r increases, v decreases, p increases, but must reach p_a at jet. $\therefore p(r) < p_a$ for $r > a$